

Improvement of Power Supply at Igbo-Etche Rumoukwurusi Area of Port Harcourt, Rivers State using Dynamic Voltage Restorer (DVR) Method

Igbinake, Osakpamwan¹, Sepiribo Lucky Braide² and Dikio Idoniboyeobu³

¹ Rivers State University, Port Harcourt

Received: 12 December 2019 Accepted: 1 January 2020 Published: 15 January 2020

Abstract

This project work examined power supply at Igbo-Etche Rumoukwurusi Area of Port Harcourt with the aim of improving power supply. The 33KV feeder from Elelewno substation which supplies the area was analysed using Dynamic Voltage Restorer (DVR) method. The method was used in Electrical Transient Analyzer Programme (ETAP). It was observed that load flow analysis is vital in understanding the ape rational nature of the network, by considering the following; Capacitive power, power before compensation, power after compensation, current before and after compensation, voltage drop, reactive current, supply current after compensation, losses in the distribution system and the ratio of loss without and with compensation. From the simulation there was low voltage profile and overloading of transformer along the distribution network. The voltage profile was improved by upgrading the network to standard power factor.

Index terms— power supply, loads, load evaluation, improved performance, igbo-etche rumoukwurusi, port harcourt.

1 Introduction

Power generation and distribution have continue to be problematic in Nigeria for decades in spite of efforts by successive government to improve supply and boost access to energy in Africa's most populous country and ensure viability of investment in the optimum benefits of electricity supply either for domestic usage or industrial production, as a result most households and businesses are left with no choice than to run fueled generators to supplement the intermittent supply which in turns brings about rise in cost of production (Ewald & Mohammad, 2008).

Electrical Power Quality is the degree of any deviation from the nominal values of the voltage magnitude and frequency. Power Quality problems concerning frequency deviation and voltage magnitude deviation is as a result of the presence of harmonics and voltage fluctuations. Other voltage problems are the voltage sags, short interruptions and transient over voltages. The power quality issues such as voltage sags, swells, harmonics, transients and their mitigation techniques that are suitable for different types of voltage sags, filter deign for reducing harmonic distortion and surge arrester sizing for location of transients ??Madrigal&Acha,2000).

Any interruption of the power quality would cost the efficiency of the system. In most of the cases, control of the power quality refers to the control of the voltage only. This is because in most cases voltage can be controlled more easily than current. More specifically, the quality of power can be described by some parameters such as continuity of service, variation in voltage magnitude, transient voltages and currents, harmonic content (for AC) etc..To describe the importance of power quality issues, we can say that poor power quality leads to unnecessary wastage of power and economy. It creates financial burden on the suppliers and consumers. Unstable voltage and frequency often creates disturbance in the power flow through transmission line (Pohjanheimo & Lakervi, 2000).

2 b) Statement of the Problem

The increasing emphasis on all power system has resulted in continued growth in the application of devices such as high efficiency adjustable speed motor drives and shunt capacitors for power factor correction, to reduce losses, resulting in increasing harmonic levels in power systems. The end users have an increased awareness of power quality issues which has led to the following: 1. Voltage fluctuation due to over/under voltage flickering of lightning causes load switching.

a) Background of the Study the problem of electricity supply in Nigeria by the Nigerian power sector is as a result of its inability to provide adequate electricity supply to domestic household and industrial producers despite a rapidly growing economy, irrespective of the country's large deposit of natural resources which can be harness and utilize for power generation. This deficiency has adverse effect on agricultural and industrial development which in turns impedes Nigeria's ongoing economic growth.

2. Voltage sag due overloading problems, intermittent lock-up causes faults in the system excessive network loading and source voltage variation. 3. Voltage swell due to data loss, damage of equipments causes start/start of heavy loads, inrush current and inadequate wiring. 4. Long time voltage interruption due to malfunction in data processing equipment causes failure of protection devices and insulation failures or control malfunction.

3 c) Aim of the Study

The research is aimed at Improving the Power Supply at Igbo-Etche Rumoukwurusi Area of Port Harcourt, Rivers State using Dynamic Voltage Restorer (DVR) method.

4 d) Objective of the Study

The objectives of this research work are:

5 e) Scope of the Study

The scope of this research work shall be limited to 33kV distribution network in Igbo-Etche Rumoukwurusi area of Port Harcourt, and to find a suitable technical solution to the factors that has adversely affected the reliability and quality of power supply to the distribution system. The scope of this research is limited to areas covered by power supply system at Igbo-Etche Rumoukwurusi Township 33KV distribution network, Rivers State. The study focuses on the Bus input and line input data as well as the power supply capacity of the distribution transformer rating in the Network. The capacity condition on the distribution transformers are needed by the Elelenwo Substation in charge of electrical power distribution in the study zone

6 f) Significant of the Study

The Significance of the research work are as follows:

1. To investigate the mentioned power quality problems.
 2. How they can be mitigated with the custom power device introduced.
 3. More details about the mitigation device would also be given, in terms of their composition and design; and also how they will be configured in an electrical system.
- II.

7 Literature Review a) Power Quality Production

Power quality is anything that affects the voltage, current and frequency of power being supplied to the customers. Constant voltage is the prime requirement of the customer because if the voltage is lower than the tolerable limits it will cause over heating of the equipment and less illuminating power to the lighting load. If it is higher than the limit it cause material insulation break down, reduces the life of lighting load etc. Lightening (transient over voltages), switching over voltages (i.e capacitor switching, disconnection of lines), short circuit faults (such as voltage sags) and short interruptions are the main causes for voltage deviations which lead to permanent damage of the equipments. Power system frequency is related to the balance between power generation and the load (Ray, 2001). When this balance changes, small change in frequency occurs. The frequency variations that go beyond acceptable limits for normal steady state operation of power system are normally caused by fault on the transmission lines, large portion of load being disconnected, or a large source of generation being isolated. Drop in frequency could result high magnetizing currents in induction motors and transformers, causing problem of overheating and saturation. Off nominal frequency will cause damage to turbine and generator due to high vibration of turbine blades which causes protection to trip out. Therefore it is essential requirement to maintain frequency of the system within the tolerable limits.

As stated by Wang & Mamishev, (2003), nowadays due to more sensitive nature of loads use of custom power devices/custom controllers (electronics based) to maintain power quality has become essential. As custom power controllers are used for current interruptions and voltage regulations, their utilization in the industry saves its equipments from voltage sags and interruptions which lead to loss of production (Madrigal, & Acha, 2000).

8 b) Protective Devices

Power systems contain protective devices to prevent injury or damage during failures. The quintessential protective device is the fuse. When the current through a fuse exceeds a certain threshold, the fuse element melts, producing an arc across the resulting gap that is then extinguished, interrupting the circuit. Given that fuses can be built as the weak point of a system, fuses are ideal for protecting circuitry from damage. Fuses however have two problems: First, after they have functioned, fuses must be replaced as they cannot be reset. This can prove inconvenient if the fuse is at a remote site or a spare fuse is not on hand. And second, fuses are typically inadequate as the sole safety device in most power systems as they allow current flows well in excess of that that would prove lethal to a human or animal ??

9 d) Overhead Transmission

High voltage overhead conductors are not covered by insulation. The conductor material is nearly always an aluminum alloy, made into several strands and possibly reinforced with steel strands. Copper was sometimes used for overhead transmission, but aluminum is lighter, yields only marginally reduced performance and costs much less. Overhead conductors are a commodity supplied by several companies worldwide. Improved conductor material and shapes are regularly used to allow increased capacity and modernize transmission circuits. Conductor sizes range from 12 mm² to 750mm² with varying resistance and current-carrying capacity. Thicker wires would lead to a relatively small increase in capacity due to the skin effect (which causes most of the current to flow close to the surface of the wire). Because of this current limitation, multiple parallel cables (called bundle conductors) are used when higher capacity is needed. Bundle conductors are also used at high voltages to reduce energy loss caused by corona discharge.

Today, transmission level voltages are usually considered to be 132 kV and above. Lower voltages, such as 66 kV and 33 kV, are usually considered sub-transmission voltages, but are occasionally used on long lines with light loads. Voltages less than 33 kV are usually used for distribution. Voltages above 765 kV are considered extra high voltage and require different designs compared to equipment used at lower voltages (Guarnieri, 2013).

Since overhead transmission wires depend on air for insulation, the design of these lines requires minimum clearances to be observed to maintain safety. Adverse weather conditions, such as high wind and low temperatures, can lead to power outages. Wind speeds as low as 23 knots (43 km/h) can permit conductors to encroach operating clearances, resulting in a flashover and loss of supply. Oscillatory motion of the physical line can be termed gallop or flutter depending on the frequency and amplitude of oscillation.

10 e) Voltage Sag

IEEE definition of voltage sag is sudden and short duration reduction in RMS value of the voltage at the point of electrical system between 0.1 to 0.9 Pu with duration from 0.5 cycles to 1 minute. The amplitude of voltage sag is the remaining value of the voltage during sag. Voltage sags are considered the most severe disturbances to industrial equipment (Acha et al., 2001). In case of semiconductor industry, voltage sag of 75% (of the nominal voltage) with duration shorter than 100ms results in material loss in the range of thousands of U.S dollars (Wang& Mamishev, 2003).

11 Materials and Methods

This chapter explained the various procedures and techniques adopted in carrying out this research work. In the process the surge impedance loading of 132KV and 33KV lines was calculated and it was use to estimate the maximum power that can be transfer by the transmission line.

12 a) Materials Used in the Analysis

Starting from the generating station to the end users, voltage is needed to be stepped up and down several times in various substations, this ensures efficient transmission of power and minimizes the power losses.

At the substation, power factor is corrected and voltage is stepped down to 33KV which is then transferred to the distribution system (feeders). (TCN 2019).

13 c) Operating Principle of Dynamic Voltage Restorer method (DVR)

The single phase DVR is employed for low power loads while three phase DVR is employed for all practical high power applications as in industrial loads and domestic loads. The basic function of the DVR is to inject a dynamically controlled voltage VDVR generated by a force commutated converter in series to the bus voltage by means of a boost transformer. The momentary amplitudes of the three injected phase voltages are controlled such as to eliminate any detrimental effects of a bus fault to the load voltage ?? ?? . This means that any differential voltages caused by transient disturbances in the ac feeder will be compensated by an equivalent voltage generated by the converter and injected on the medium voltage level through the boost transformer. The DVR works independently of the type of fault or any event that happens in the system, provided that the whole

system remains connected to the supply grid, i.e. the line breaker does not trip. For most practical cases, a more economical design can be achieved by only compensating the positive and negative sequence components of the voltage disturbance seen at the input of the DVR. This option is reasonable because for a typical distribution bus configuration, the zero sequence part of a disturbance will not pass through the step down transformer because of infinite impedance for this component. The DVR has two modes of operation which are: standby mode and boost mode. In standby mode (VDVR=0), the boost transformer's low voltage winding is shorted through the converter. No switching of semiconductors occurs in this mode of operation, because the individual converter legs are triggered such as to establish a short-circuit path for the transformer connection. Therefore, only the comparatively low conduction losses of the semiconductors in this current loop contribute to the losses. The DVR will be most of the time in this mode. In boost mode (VDVR>0), the DVR is injecting a compensation voltage through the booster transformer due to a detection of supply voltage disturbance. The capacitive power can be determinate when the power and current before and after compensation is required:

The power and current before compensation are: Scenario 3: To Determine the Cable Cross-Section of the Network A three phase power of 4250kW, with $V_L = 415V$, at 50 Hz is to be transmitted over a cable 80m in length, the voltage drop must not exceed 4% = 16.6V. The power factor is to be increased from $\cos \phi = 0.84$ to $\cos \phi = 0.91$. $I = \frac{P}{\sqrt{3} \times V_L \times \cos \phi} = \frac{4250}{\sqrt{3} \times 415 \times 0.84} = 5059.52A$

14 P = ?3. ? ? ? ? ? ? ? ? ?

Where: P = Effective Power V_L = Rated Voltage f = Frequency I_1 = Current consumption before compensation I_2 = current consumption after compensation $\cos \phi$ = Power factor The current consumption before compensation is: $I_1 = \frac{P}{\sqrt{3} \times V_L \times \cos \phi} = \frac{4250}{\sqrt{3} \times 415 \times 0.84} = 5059.52A$

The current consumption after compensation is: $I_2 = \frac{P}{\sqrt{3} \times V_L \times \cos \phi} = \frac{4250}{\sqrt{3} \times 415 \times 0.91} = 4697.7A$

The effective resistance per unit length before compensation for 7.04 A is ($R = \frac{V}{I} = \frac{16.6}{7.04} = 2.358 \Omega/km$)

The effective resistance per unit length after compensation for 6.49 A is ($R = \frac{V}{I} = \frac{16.6}{6.49} = 2.559 \Omega/km$)

15 e) Voltage Divider Model

Voltage divider model is used for the calculation of voltage sag magnitude in case of sag due faults at the point of common coupling (PCC) in the radial system. In this case voltage V_L during fault can be expressed as: $V_L = \frac{V_{PCC} \times Z_{fault}}{Z_{PCC} + Z_{fault}}$ (3.1)

Where: Z_{PCC} is the impedance of the grid Z_{fault} is the impedance between the PCC and the fault including fault and line impedances V_L is the supply voltage

Voltage sag is also related to the changes in voltage phase angle. This change in phase angle is also called as phase angle jump (i.e the phase angle between during sag and pre-sag voltages) and is obtained by taking argument of the complex of voltage V_L .

Assuming the load voltage and current in prefault conditions equal to 1 Pu, the injected power by the device during voltage sag mitigation is equal to $P = V_L \times I \times \cos \phi$ (3.2)

The Euler identity can be written as $e^{j\theta} = \cos \theta + j \sin \theta$, applying to (3.2) we get $P = V_L \times I \times (\cos \theta + j \sin \theta)$ (3.3)

Power absorbed by the load will be given by The purpose of showing equations (3.5) and (3.6) is to show the dependency of active and reactive power injection by DVR on certain factors. These equations show that these powers depends on sag depth, phase angle jump, load angle and load active and reactive powers. $P = V_L \times I \times \cos \theta$ (3.4)

16 f) Voltage Controller

In this section the outer loop proportional voltage controller will be derived. Some basic assumptions before deriving is that the injected voltage is equal to the voltage across the capacitors of the VSC output filter, i.e. the injection transformer is considered ideal with a 1:1 turn ratio, therefore $V_{inj} = V_{VSC}$ (3.7)

and is the same for other two phases With a PLL synchronized with the grid voltage vector we can transform from $\alpha\beta$ to dq coordinate system, which will give us the dc values in steady state and thus easier to implement a control system. This is the basic tool of vector control. We get the equation (3.16) that is the plant for which we want to design a controller. As the plant is a first order system, so we will use first order Low Pass Filter (LPF) response for the design of the voltage controller.

17 g) An unbalanced 3-phase system

An unbalanced 3-phase system consists of positive, negative, and zero sequence fundamental and harmonic components. The system voltage can be expressed as in equation (3.17):

$$V(t) = V_0(t) + V_1(t) + V_2(t) + V_3(t) + \dots$$
 (3.17) Here subscripts +, -, and 0 represent positive, negative and zero sequence components respectively. The series converter compensates for the following components of voltage:

$$V_0(t) = V_0(t) + V_1(t) + V_2(t) + V_3(t) + \dots$$
 (3.18) Control system automatically controls the series converter so that the output converter voltage is $V_0(t)$. The nonlinear load current (equation (3.9)) with distortion can be expressed as:

$$i(t) = I_0(t) + I_1(t) + I_2(t) + I_3(t) + \dots$$
 (3.19) The shunt converter provides compensation of the load harmonic currents to reduce voltage distortion. Output current with harmonic, negative and zero sequence currents controls the shunt converter so that load current distortions can be nullified. The current component which is compensated by the shunt converter is given by equation (3.20):

$$I_0(t) = I_0(t) + I_1(t) + I_2(t) + I_3(t) + \dots$$
 (3.20) Equation (3.18) and equation (3.20) establish the basic principles of an ideal Unified Power Quality Controller (UPQC).

18 h) Determination of power and current after compensation

The power and current after compensation are:

$$P = P_0 + P_1 + P_2 + P_3 + \dots$$
 (3.21)
$$I = I_0 + I_1 + I_2 + I_3 + \dots$$
 (3.22)

The required capacitive power is: $P_c = P \tan \phi - P \tan \phi_c$ (3.23) where; P = effective power, ϕ = power factor is to be compensated, ϕ_c = Determination of cable cross-section A three phase power is given with in respect of the rated voltage, frequency is to be transmitted over a cable with different length, the voltage drop is given and must not exceed some percentage level. The power factor is to be increased between the existing pf and improved pf. The power is expressed mathematically:

$$P = \frac{W}{t}$$
 (3.25) Where: P = effective power, V = Rated Voltage The current consumption before compensation is:

$$I = \frac{P}{V}$$
 (3.26) The current consumption after compensation is:

$$I = \frac{P}{V}$$
 (3.27) The effective resistance per unit length before and after compensation is expressed as:

$$R = \frac{V}{I}$$
 (3.28) A single phase load is fed from an AC supply with an Input AC of a given voltage with frequency in Hz and a base impedance. It is to be realized as a unity power factor load on the AC supply system using shut connected lossless passive element (L or C).

The load current before compensation is given as the supply voltage per load impedance, which is expressed mathematically:

19 i) How Installing Power Capacitors Improve System

Operating Characteristics (Reduce Line Losses) Improving Pf at the load point shall relieve the system of transmitting reactive current. Less current shall mean lower losses in the distribution system of the facility since losses are proportional to the square of the current. Therefore, the fewer kW-hr needed to be purchased from the utility.

An estimation of the power losses can be made using the following: % reduction in power losses =

$$\frac{P_{loss} - P_{loss}'}{P_{loss}} \times 100$$
 (3.33) The value of the capacitor for power factor correction is expressed as:

$$C = \frac{P}{V^2 \omega (\tan \phi - \tan \phi_c)}$$
 (3.34) The supply current after compensation is expressed as:

$$I = \frac{P}{V}$$
 (3.35) The equivalent resistance of the compensated load is expressed as:

20 Determination of Losses in the Distribution System

A single phase AC Voltage controller is used to control the heating of packing element in a machine at a given power with respect to voltage which is fed from a single-phase AC mains at a frequency of 50Hz. Feeder conductors have the resistance of where is fed from the network. The rms voltage across the load is

21 Determination of Reduction of Voltage Drop

$$V_d = I R$$
 (3.41)

The supply rms current is:

$$I = \frac{P}{V}$$
 (3.42) Losses in the distribution system are:

$$P_{loss} = I^2 R$$
 (3.43) Ratio of losses without and with a compensator is (3.46) Where it has been assumed that the pre-event voltage is exactly 1 pu, thus $E = 1$. We see from equation (3.46) the sag becomes deeper for faults electrically closer to the customer (when z becomes smaller), and for systems with a smaller fault level (when z becomes larger).

Equation (3.47) can be used to calculate the sag magnitude as a function of the distance to the fault. Therefore we have to write $z = z \times z$, with z the impedance of the feeder per unit length and z the distance between the fault and the pcc, leading to:

22 Determination of Fault Levels

It is possible to calculate the sag magnitude from the fault levels at the pcc and at the fault position. Let V_{f} be the fault level at the fault position and V_{pcc} at the point-of-common coupling. For a rated voltage V_r the relations between fault level and source impedance are as follows: $V_{f} = V_r^2 / (Z_s + Z_f)$ (3.48) $V_{pcc} = V_r^2 / (Z_s + Z_{pcc})$ (3.49)

with equation (3.47) the voltage at the pcc can be written as: $V_{pcc} = 1 - \frac{Z_{pcc}}{Z_s} V_{f}$ (3.50)

23 j) Newton-Raphson Power Flow Technique (N-R)

Newton-Raphson technique is used for solving power flow solution. The technique uses Taylor series expansion with terms limited to first approximation. The technique was used in this research due to its powerful convergence characteristics compared to other techniques.

Complex power at the i th node on the distribution line is given by Where: Y_{ik} is the admittance matrix V_i is the injected real power Q_i is the injected reactive power. $P_i = V_i^2 \sum_{k=1}^n G_{ik} - V_i \sum_{k=1}^n V_k Q_{ik} \sin \theta_{ik}$ (3.51) IV.

24 Results and Discussion

25 a) Description of the Research Work

This chapter analyses the performance of the Dynamic Voltage Restorer (DVR) with different techniques by determining the capacitive power of the network, % reduction in power loss of the network, cable cross-section of the network, compensation of the network, losses in the distribution system of the network, reduction of voltage drop of the network, faults behind the transformer of the network. The different techniques were analyzed in tabular form and bar chart was used to discuss results of the scenarios. The use of Electrical Transient and Analysis Program Software (ETAP version 12.6) was used in analyzing the possible solutions to improved power supply. For the reactive power, Residential Estate I has the highest value of the active power of 3500 kVAR, followed by Total Energy Limited with active power of 3150 kVAR. While Favour Avenue has the lowest values of 250.50kVAR.

For the apparent power, Total Energy Limited has the highest value of the active power of 5290.09 kVA, followed by Residential Estate I with active power of 4803.33kVA. While Winderville 1 has the lowest values of 604.38kVA.

Therefore for active power Winderville 1 and Winderville 3 should be upgraded and the active power should be increased.

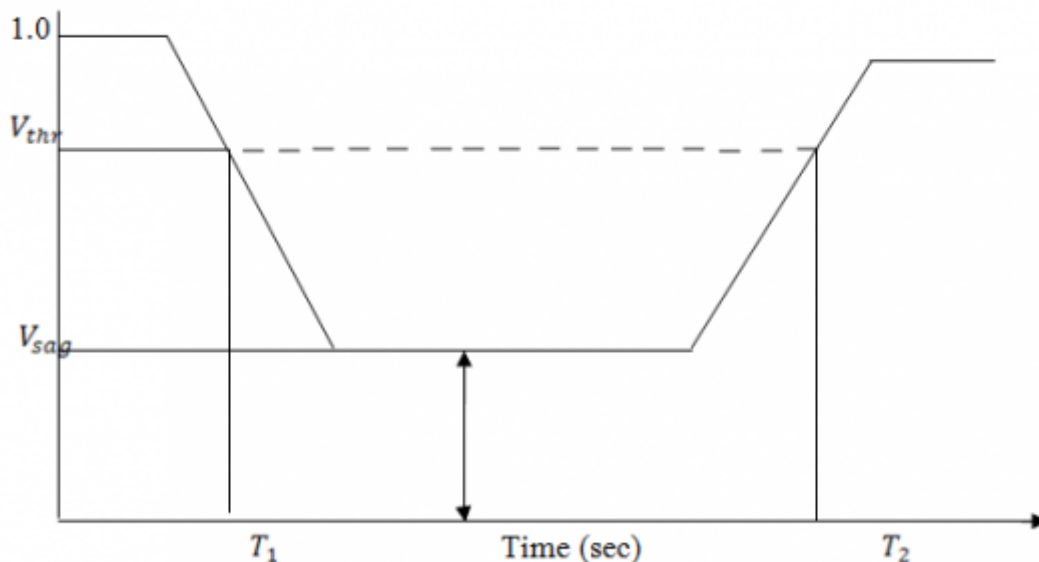
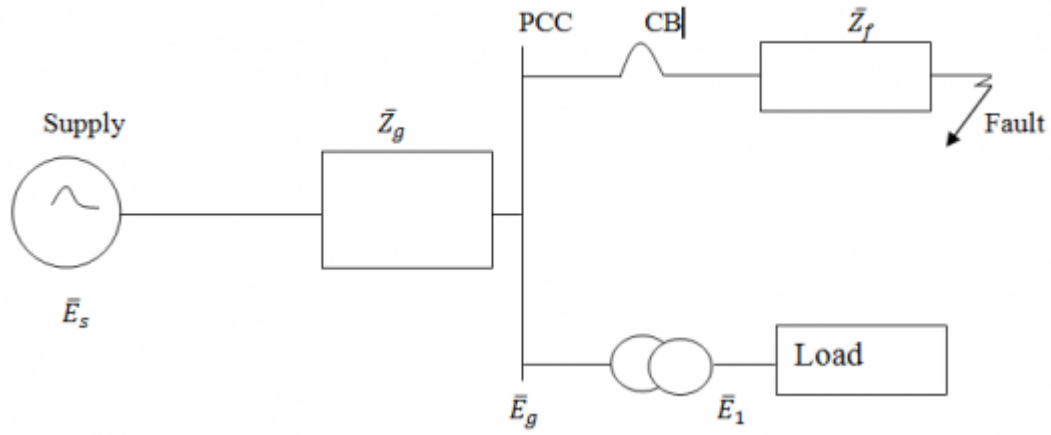


Figure 1: 1 .

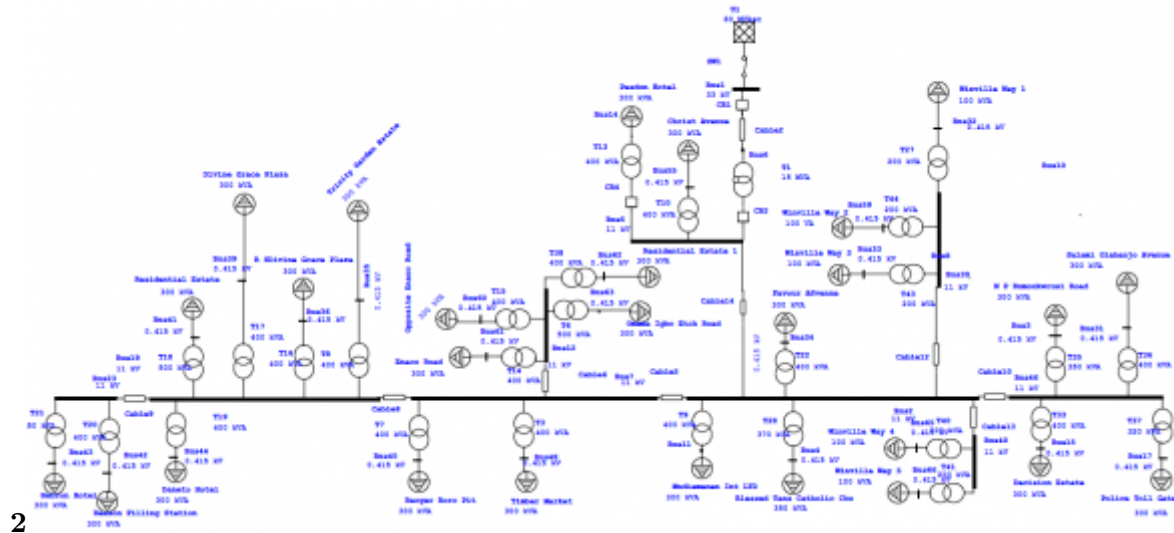
¹Improvement of Power Supply at Igbo-Etche Rumoukwurusi Area of Port Harcourt, Rivers State using Dynamic Voltage Restorer (DVR) Method © 2020 Global Journals

²© 2020 Global Journals



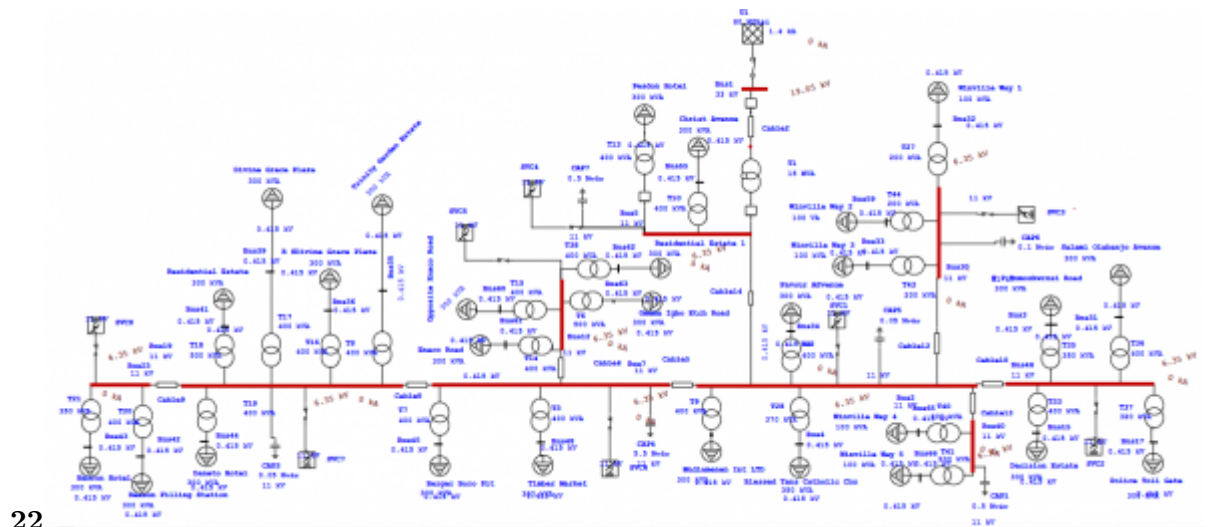
21

Figure 2: Figure 2 . 1 :



2

Figure 3: Figure 2 .



22

Figure 4: Figure 2 . 2 :

31

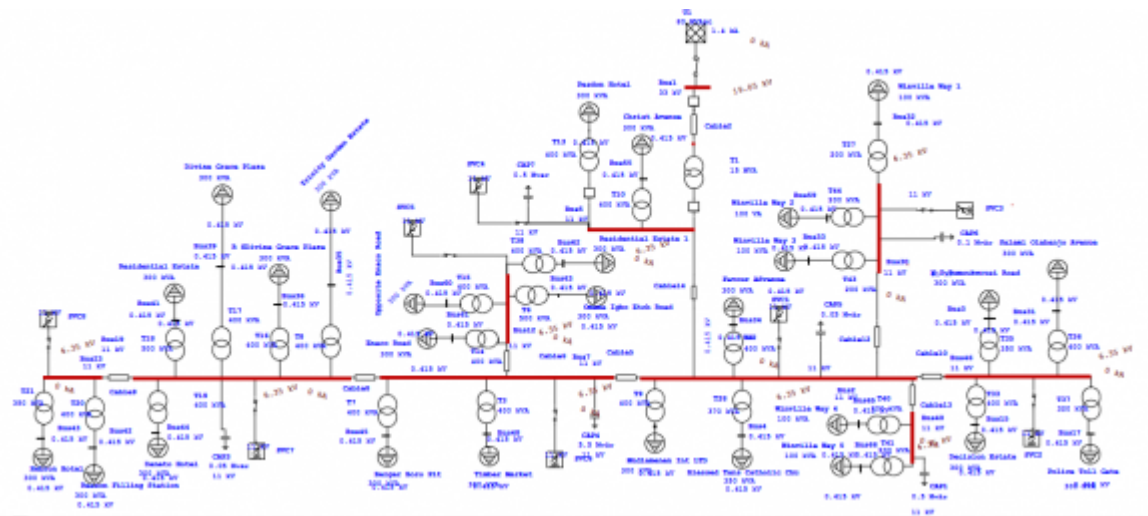


Figure 5: Figure 3 . 1 :

221

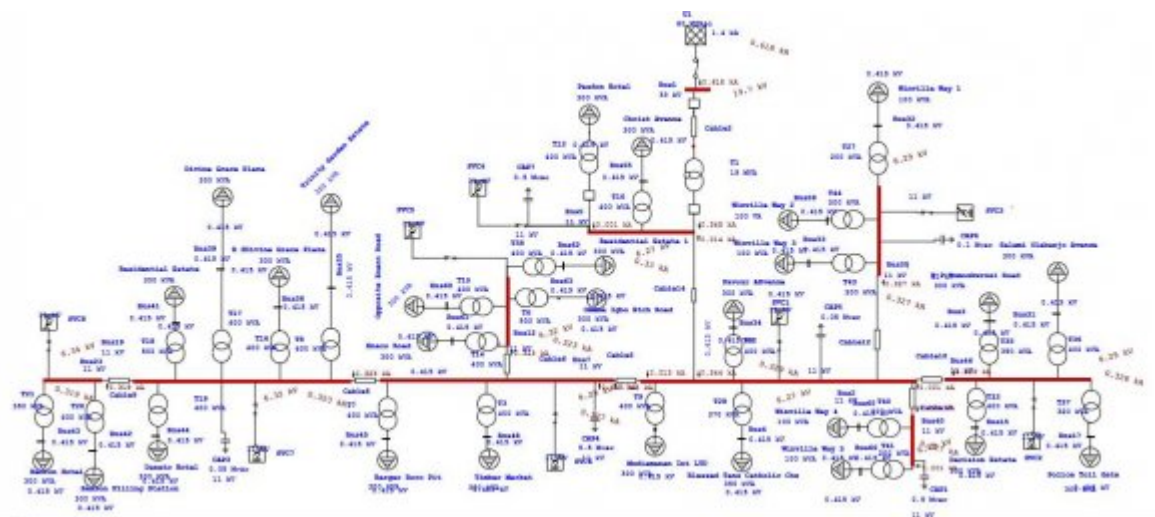


Figure 6: 2 : 2 ?= (1 ?

The 132KV/33KV substation station has six feeders viz:

1. Onne Feeder
2. Bori Feeder
3. RST Feeder
4. Timber Feeder
5. Igbo-Etchee Feeder
6. Old Oyigbo Feeder

Two sets of incoming 132KV power lines from Afam Power Generation

5. DC charging set
6. Nominal rating of distribution transformers.
7. Electrical Transient and Analysis Program (ETAP Version 12.6)

8. Igbo-Etche Rumoukwurusi Road load data from Port Harcourt Electricity Distribution Total Energy Limited (PHED).

9. Igbo-Etche Rumoukwurusi Road Distribution Network single line diagram

b) Description of Igbo-EtcheRumoukwurusi Road 33kV

Distribution Network

1. Injection transformer
2. Harmonic/Passive filter
3. Storage devices/Energy storage systems
4. Voltage source converter

The Igbo-Etche Rumoukwurusi distribution network is fed by Elenwo Substation (132KV/33KV), the substation consists of two 60MVA transformers (2 x 60MVA transformer).

Figure 7:

$U(t)$ C $??$ $??$
 $(??)$

Figure 3.2: Single line View of LC filter and ideal VSC Now by applying Kirchhoff's Current Law to the LC

© 2020
 Global
 Jour-
 nals

Figure 8:

$??$ $??$ (3.45)
 $??$

Determination of Voltage Divider Model for a Voltage Sag

Voltage divider model for a voltages ag

$??$ $?????? =$ $??$ $??$
 $??$ $??$
 $+??$ $??$

Year 2020
 of Researches in Engineering () Volume
 XX Issue V Version I F
 Global Journal
 $??$ $????????$ $??$ $????????????$ (3.44)
 © 2020 Global Journals

Figure 9:

$$I \cos \phi = \frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.54)$$

$$I \sin \phi = \frac{V I \sin \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.55)$$

$$I \cos \phi = \frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.56)$$

$$I \sin \phi = \frac{V I \sin \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.57)$$

Where:

i is node 1,2,3,4,5,6,7+?.. on the distribution line

Determination of Injected Real and Reactive Power

From (3.52) the current entering the power system is giving by

$$I \cos \phi = \frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.58)$$

$$\text{Let } I \cos \phi = \frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}} \quad (3.59)$$

$$\text{Separating (3.62) into real and imaginary parts we have,} \quad (3.60)$$

$$\begin{aligned} I \cos \phi &= \frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}} \\ I \sin \phi &= \frac{V I \sin \phi}{2 \sqrt{1 + \tan^2 \phi}} \end{aligned} \quad (3.61)$$

[Note: * = $\frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}}$ + $\frac{V I \sin \phi}{2 \sqrt{1 + \tan^2 \phi}}$] (3.60) $\frac{V I \cos \phi}{2 \sqrt{1 + \tan^2 \phi}}$ + $\frac{V I \sin \phi}{2 \sqrt{1 + \tan^2 \phi}}$] (3.63)]

Figure 10:

(kW) Reactive Power (kVar) Apparent Active, Active Power Power (kVA)
Existing

Figure 11: Reactive and Apparent Power Bus Location Variation of Active, Reactive, Apparent Power with respect to Bus Location

Year 2020

I

Global Journal of Researches in Engineering () Volume % Existing Power Factor
XX Issue V Version F % Improved Power Fac-

tor

© 2020 Global Journals

Figure 12: and Improved Power Factor Bus Location Variation of Existing and Improved Power Factor with respect to Bus Location

For improved power factor, Winderville 1 has the highest value of 92.5. Followed by New Pipeline Rumoukwurusi, Favour Avenue and Ngre Oil Filling Station with the value of 92.3 respectively. While Mecho Estate / Trinity Garden Estate and Police Toll Gate have lowest value of 90 respectively.

Mecho Estate/Trinity Garden Estate should be upgrade to the standard power factor as 85.0 since it is a residence area.

.1 V. Conclusion and Recommendations

.2 a) Conclusion

This research work critically examined the improvement of power supply at Igbo-Etche Rumoukwurusi Area of Port Harcourt, Rivers State using Dynamic Voltage Restorer (DVR) method.

Based on the results obtained, it can be concluded that load flow analysis is very vital for understanding the operational nature of a network and the following area were considered vigorously; the capacitive power, power before compensation, power after compensation, current before and after compensation, % reduction in power loss, voltage drop, current consumption before and after compensation, load current before compensation, reactive current, capacitive for pf correction, current after compensated load and resistance of the compensated load, Supply r ms Current, Voltage across the load, Load Resistance, Supply current after compensation, Losses(fixed) in the distribution system, Losses(variable) in the distribution system and Ratio of losses without and with a compensator.

Similarly, distance between the fault, source impedance, transformer impedance, rated voltage, fault level at the fault position, point of common coupling and the voltage sag with respect to Bus Location were considered.

However, the use of Electrical Transient and Analysis Program (ETAP Version 12.6) and was used for simulation of the case study. Post-upgrade simulation was conducted on the network to ascertain the improvement of power supply on the network and the results were significantly positive.

.3 b) Contribution to Knowledge

While other works focused on various power quality problems faced by the utilities such as harmonic distortion and different disturbances, other devices like D-STATCOM (distribution static compensator) which is represented by FACTS devices is used in power system as power electronic shunt device that absorbs and provides reactive power to solve power quality problems in power distribution systems, this work has considered the Power quality is the combination of voltage quality and current quality. Power quality is the set of limits of electrical properties that allows electrical systems to function in their intended manner without significant loss of performance or life.

.4 c) Recommendations

Based on the findings of this work, the following recommendations are made to ensure the overall improvement in the operation of the network:

[Nielsen and Blaabjerg ()] ‘A detailed comparison of system topologies for dynamic voltage restorers, Industry Applications’. G Nielsen , F Blaabjerg . *IEEE Transactions on* 2005. 41 (5) p. .

[Li et al. ()] ‘A dual-functional medium voltage level DVR to limit downstream fault currents’. Y W Li , M Vilathgamuwa , D P Chiang Loh , F Blaabjerg . *Power Electronics, IEEE Transactions*, 2007. 22 p. .

[Newman et al. ()] ‘A dynamic voltage restorer (DVR) with selective harmonic compensation at medium voltage level, Industry Applications’. M J Newman , D G Holmes , J G Nielsen , F Blaabjerg . *IEEE Transactions* 2003. 41 (6) p. .

[Lee et al. ()] ‘A novel control algorithm for static series compensators by use of PQR instantaneous power theory’. S J Lee , H Kim , S K Sul . *IEEE Trans on Power Electronics* 2004. 19 (3) p. .

[Yash et al. ()] ‘A Review of Compensating Type Custom Power Devices for Power Quality Improvement’. P Yash , A Swarup , S Bhim . *IEEE Power India Conference* 2008. 5 (9) p. .

[Daniel and Ambra ()] ‘A Summary of the Draft IEEE P1409 Custom Power Application Guide” Transmission and Distribution Conference and Exposition’. D Daniel , S Ambra . *IEEE PES* 2003. 3 (7) p. .

[Chan et al. ()] *Boundary controller for dynamic voltage restorers to achieve fast dynamic response*, K Chan , K Leung , H Chung , S Hui . 2006.

[Wang and Mamishev ()] ‘Classification of Power Quality Events Using Optimal Time Frequency representation’. M Wang , V Mamishev . *IEEE Transactions on Power Delivery* 2003. 18 (9) p. . (Part 2: Application)

[Ghosh and Ledwich ()] ‘Compensation of distribution system voltage using DVR’. A Ghosh , G Ledwich . *IEEE Transactions on* 2002. Power Delivery. 17 (4) p. .

[John and Frede ()] ‘Control Strategies for Dynamic Voltage Restorer Compensating Voltage Sags with Phase Jump’. G John , B Frede . *Applied Power Electronics Conference and Exposition*, 2001. IEEE. 2 p. .

[Pillay and Manyage ()] ‘Definitions of Voltage Unbalance’. P Pillay , M Manyage . *IEEE Power Engineering Review* 2001.

- [Jowder ()] 'Design and analysis of dynamic voltage restorer for deep voltage sag and harmonic compensation'. F A Jowder . *Generation, Transmission & Distribution* 2009. 3 (7) p. .
- [Paisan et al. ()] *Detailed Analysis of Load Voltage Injection for Dynamic Voltage Restorers* TENCON, B Paisan , M Nadarajah , K Rajamangala . 2006. 12 p. . (University of Technology Thanyaburi Thailand. IEEE region 10 conference)
- [Tiwari and Sunil ()] 'Dynamic Voltage Restorer against Voltage Sag'. H Tiwari , G Sunil . *International Journal of Innovation* 2010. 1 (3) p. . (Management and Technology.)
- [Omar et al. ()] 'Dynamic Voltage Restorer Application for Power Quality Improvement in Electrical Distribution System: An Overview'. R Omar , N Rahim , M Sulaiman . *Australian Journal of Basic and Applied Sciences* 2011. 5 (12) p. .
- [Roncero-Sanchez and Acha ()] 'Dynamic voltage restorer based on flying capacitor multilevel converters operated by repetitive control, Power Delivery'. & P Roncero-Sanchez , E Acha . *IEEE Transactions on* 2009. 24 (2) p. .
- [Zhan et al. ()] 'Dynamic voltage restorer based on voltage space vector PWM control'. C Zhan , V Ramachandaramurthy , A Arulampalam , C Fitzer , S Kromlidis , M Barnes , N Jenkins . *Applied Power Electronics Conference and Exposition*, 2001. 2001. 2001. APEC. 2 p. .
- [Pakharia and Gupta ()] 'Dynamic Voltage Restorer for Compensation of Voltage Sag and Swell: A Literature Review'. A Pakharia , M Gupta . *International Journal of Advance in Engineering & Technology* 2012. 4 (1) p. .
- [Chapman ()] *Electric Machinery and Power System Fundamentals*, S Chapman . 2002. Boston: McGraw-Hill.
- [Grigsby ()] *Electric Power Generation, Transmission, and Distribution*, L Grigsby . 2007. 2007. CRC Press.
- [Bollen ()] *Electric Power Systems Research*, M J Bollen . 2003. 66 p. . (What is power quality?)
- [Roger et al. ()] *Electrical Power Systems Quality*, C Roger , F Dugan , M Mcgranaghan . 2002. McGraw-Hill. (Professional Engineering)
- [Dugan et al. ()] *Electrical Power Systems Quality second edition*, R C Dugan , M F Mcgranaghan , S Santoso , H Wayne . 2002. New York: McGraw-Hill.
- [Acha et al. ()] *Electronic Control in Electrical Power Systems*, E Acha , V Agelidis , O Anaya-Lara , J Miller . 2001. London, U.K., Butterworth-Heinemann.
- [Woodley et al. ()] 'Experience with an inverter-based dynamic voltage restorer'. N Woodley , L Morgan , A Sundaram . *Electrical & Computer Engineering: An International Journal (ECIJ)* 2015. 1999. 14 (3) p. 95. (IEEE Transactions on)
- [Padiyar ()] *Facts controllers in power transmission and distribution* new age international (P) Ltd publishers, K Padiyar . 2007.
- [IEEE Standard Dictionary of Electrical and Electronic Terms] IEEE Standard 100-1992. *IEEE Standard Dictionary of Electrical and Electronic Terms*,
- [Ogbu et al. ()] 'Improved Performance of 132kv Transmission Line of Afam Power Station to Elelenwo Substation, Port Harcourt'. I Ogbu , D Idoniboyeobu , S L Braide . *International Journal of Scientific & Engineering Research* 2018. 9 (11) p. .
- [David et al. ()] 'Improving Power Quality'. H David , U David , N Damir , K Steven , L Carl , T Marco . *ABB Review* 2010. 4 (8) p. .
- [El-Mofty and Youssef ()] 'Industrial power quality problems'. A El-Mofty , K Youssef . *Electricity Distribution, Part 1: Contributions. CIRED.16th International Conference and Exhibition on (IEE Conf*, 2001. 2.
- [John and Alan ()] *Introduction to Power Quality* power engineering journal, S John , C Alan . 2001. 8 p. .
- [Masoud ()] A Masoud . *Power Quality in Electric Networks: Monitoring and Standards* the second world engineering conference, 2002. 8 p. .
- [Vilathgamuwa and Wijekoon ()] *Mitigating Zero Sequence Effects in Dynamic Voltage Restorers*, M Vilathgamuwa , H Wijekoon . 2007. 2007. IEEE. 17 p. . (Power Electronics Specialists Conference, PESC)
- [Omar and Rahim ()] 'Modeling and simulation for voltage sags/swells mitigation using dynamic voltage restorer (DVR)'. R Omar , N A Rahim . *Power Engineering Conference, 2008. AUPEC '08. Australasian Universities*, 2008. 1 p. .
- [Fawzi ()] 'Modeling and Simulation of Different System Topologies for Dynamic Voltage Restorer'. J Fawzi . *EPECS '09. International Conference*, 2009. 9 p. . (Electric Power and Energy Conversion Systems)
- [Madrigal and acha ()] *Modelling of Custom Power Equipment Using Harmonic Domain Techniques*, M Madrigal , E &acha . 2000. IEEE.
- [Stones and Collinson ()] 'Power quality'. J Stones , A Collinson . *Power Eng. Journal* 2001. (2) p. .

- [Benachaiba and Ferdi ()] ‘Power Quality Improvement Using DVR’. C Benachaiba , B Ferdi . *American Journal of Applied Sciences* 2009. 6 (3) p. .
- [Ewald and mohammad ()] *Power Quality in Power Systems and Electrical Machines*, F Ewald , A &mohammad . 2008. Burlington, USA: Elsevier Academic Press.
- [Mahesh et al. ()] *Rating and design issues of DVR injection transformer*, S Mahesh , M Mishra , B Kumar , V Jayashankar . 2008. p. .
- [Babaei and Kangarlu ()] *Sensitive load voltage compensation against voltage sags/swells and harmonics in the grid voltage and limit downstream fault currents using DVR*, *Electric Power Systems Research*, E Babaei , M F Kangarlu . 2012. 83 p. .
- [Ray ()] *Solutions to Power Quality Problems” power engineeringjournal*, A Ray . 2001. p. .
- [Flores ()] ‘State of the Art in the Classification of Power Quality Events, AnOverview’. R Flores . *Harmonics and Quality of Power*, 2002. 2002. 1 p. . (th International Conference)
- [Pohjanheimo and Lakervi ()] ‘Steady state modeling of custom power components in power distribution networks’. P Pohjanheimo , E Lakervi . *IEEE Power Engineering Society Winter Meeting* 2000. 5 (8) p. .
- [Ramachandaramurthy et al. ()] ‘Supervisory control of dynamic voltage restorers’. V Ramachandaramurthy , A Arulampalam , C Fitzer , C Zhan , M Barnes , N Jenkins . *IEE Proc.-Gener. Transm. Distrib* 2002. 151 (4) p. .
- [Guarnieri ()] ‘The Beginning of Electric Energy Transmission: Part One’. M Guarnieri . 10.1109/MIE.2012.2236484. *IEEE Industrial Electronics Magazine* 2013. 7 (1) p. .
- [Michael et al. ()] ‘The role, of custom power products in enhancing power quality at industrial facilities’. D Michael , G Stump , J Keane . *International Conference*, 1998. 6 p. .
- [Hingorani and Gyugyi ()] *Understanding FACTS -Concepts and Technology of Flexible AC Transmission Systems*, N Hingorani , L Gyugyi . 2000. New York: IEEE Press.
- [Bollen ()] *Understanding Power Quality Problems-Voltage Sags and Interruptions*, M J Bollen . 2000. New York: IEEE Press.
- [Posada et al. ()] ‘Voltage compensation for common disturbances at the distribution level’. J Posada , J Ramirez , R Correa . *IEEE PES Conference on* 2011. (16) p. . (Innovative Smart Grid Technologies (ISGT Latin America))
- [Chris et al. ()] ‘Voltage Sag Detection Techniquefor a Dynamic Voltage Restore’. F Chris , B Mike , G Peter . *IEEE Transactions on Power Delivery* 2004. 40 (1) p. .
- [Bollen ()] ‘Voltage sags in three-phase systems’. M J Bollen . *Power Engineering Review, IEEE* 2001. 21 (15) p. .